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MULTI-MEDIA ROTATING SOOTBLOWER AND AUTOMATIC INDUSTRIAL BOILER CLEANING SYSTEM

REFERENCE TO RELATED APPLICATIONS

This application claims priority to commonly-owned United States Provisional
10 Patent Application Serial No. 60/394,599, entitled "Long Retractable Rotating Multi
Media Sootblower," filed on July 9, 2002.

TECHNICAL FIELD

The present invention relates to sootblowers used to clean industrial boilers
15 and, more particularly, relates to a multi-media rotating sootblower that includes
multiple rotating and individually controlled cleaning fluid applicators, such a set of
steam nozzles and two sets of water nozzles, and an automatic boiler cleaning
system using these sootblowers.

20 BACKGROUND OF THE INVENTION

Industrial boilers, such as oil-fired, coal-fired and trash-fired boilers in power
plants used for electricity generation and waste incineration, as well as boilers used in
paper manufacturing, oil refining, steel and aluminum smelting and other industrial
enterprises, are huge structures that generate tons of ash while operating at very high
25 combustion temperatures. These boilers are generally characterized by an enormous
open furnace in a lower section of the boiler housed within walls constructed from
heat exchanger tubes that carry pressurized water, which is heated by the furnace.
An ash collection and disposal section is typically located below the furnace, which
collects and removes the ash for disposal, typically using a hopper to collect the ash
30 and a conveyor or rail car to transport it away for disposal.

A superheater section is typically located directly above the furnace, which
includes a number of panels, also called platens or pendants, constructed from heat
exchanger tubes that hang from the boiler roof, suspended above the combustion
zone within the furnace. The superheater platens typically contain superheated
35 steam that is heated by the furnace gas before the steam is transported to steam-

driven equipment located outside the boiler, such as steam turbines or wood pulp cookers. The superheater is exposed to very high temperatures in the boiler, such as about 2800 degrees Fahrenheit [about 1500 degrees Celsius], because it is positioned directly above the combustion zone for the purpose of exchanging the heat generated by the furnace into the steam carried by the platens. The boiler also includes a number of other heat exchangers that are not located directly above the furnace, and for this reason operate at lower temperatures, such as about 1000-1500 degrees Fahrenheit [about 500-750 degrees Celsius]. These boiler sections may be referred to as a convection zone typically including one or more pre-heaters, re-heaters, superheaters, and economizers.

There is a high demand for thermal energy produced by these large industrial boilers, and they exhibit a high cost associated with shutting down and subsequently bringing the boilers back up to operating temperatures. For these reasons, the boilers preferably run continuously for long periods of time, such as months, between shut down periods. This means that large amounts of ash, which is continuously generated by the boiler, must be removed while the boiler remains in operation. Further, fly ash tends to adhere and solidify into slag that accumulates on high-temperature interior boiler structures, including the furnace walls, the superheater platens, and the other heat exchangers of the boiler. If the slag is not effectively removed while the boiler remains in operation, it can accumulate to such an extent that it significantly reduces the heat transfer capability of the boiler, which reduces the thermal output and economic value of the boiler. In addition, large unchecked accumulations of slag can cause huge chunks of slag to break loose, particularly from the platens, which fall through the boiler and can cause catastrophic damage and failure of the boiler.

The slag accumulation problem in many conventional boilers has been exacerbated in recent years by increasingly stringent air quality standards, which have mandated a change to coal with a lower sulphur content. This low-sulphur coal has a higher ash content and produces more tenacious slag deposits that accumulate more quickly and are more difficult to remove, particularly from the superheater platens. To combat this problem, the industry has developed increasingly sophisticated boiler cleaning equipment that operates continually while the boiler remains in operation. In particular, water cannons can be periodically used to clean the boiler walls in the open furnace section, and conventional steam sootblowers can be used to clean the heat exchangers. These steam sootblowers generally include

lance tubes that are inserted into the boiler adjacent to the heat exchangers and operate like large pressure washers to clean the heat exchangers with steam blasts while the boiler remains in operation.

Conventional steam sootblowers have included rotating lance tubes that blast the steam in a corkscrew pattern to clean as wide an area as possible as the lance advances. In these superheaters, the platens are typically arranged in rows of panels, and therefore require a system of sootblowers that travel among and clean the various platens. However, slag deposits in some boiler superheaters have proven to be so tenacious that this type of steam cleaning is insufficient. For areas with slag deposits that resist steam cleaning, sootblowers that use water as the cleaning medium have been employed. A difficulty arises with the use of water as a cleaning fluid because the thermal shock imposed on the heat exchanger tubes is much greater when water is used as the cleaning fluid. Eventually, water shock can cause the heat exchanger tubes to crack and fail, which requires a major boiler renovation.

Water stress is such a serious issue that water cleaning should be kept to a minimum to avoid unnecessarily shortening the boiler's life. Furthermore, water cleaning tends to cause slag to be removed from the platens in fairly large sections, as the water penetrates the slag and flashes to steam, which blows chunks of slag away from the platen. Once a large chunk of slag has been removed, it is important that the now bare platen tubes not be shocked with subsequent water streams. It is also important that water cleaning, unlike steam, not be applied too close to the heat exchanger tubes to avoid cracking the tubes during the cleaning process.

The boiler cleaning problems described above have led to the proliferation of sootblowers, particularly in the superheater areas of boilers, because steam sootblowers are desirable for regularly-scheduled cleaning passes, whereas more closely controlled water sootblowers are desirable for occasional rigorous cleaning of areas encrusted with tenacious slag that resists steam cleaning. This dual-media cleaning need has led to the advent of dual-media sootblowers that have attempted to effectively deliver both steam and water as cleaning fluids. However, the objective of delivering both steam and water through a single lance has proved difficult to attain because water lances are typically tethered to water hoses, whereas steam lances rotate freely. In addition, water lances require greater precision and control than conventional steam lances afford, for example requiring independent control of the water streams and the ability to turn the water off at a particular water jet when that jet is positioned too close to a heat exchanger tube or directed at a structure that has

already been successfully cleaned. Incorporating these capabilities into a water lance that also delivers steam as a cleaning fluid has not been successfully accomplished.

These difficulties are accentuated in the harsh environment of the interior of an operating industrial boiler. Sootblower lances can be quite long, such as 50 feet, 5 depending on the particular boiler. Metal structures, such as tubes, hoses, couplers and nozzles experience extreme heat expansion and expansion-related stresses in this type of environment. Further, the need for long periods of active duty with very low failure rates is almost as critical for the boiler cleaning equipment as for the interior components of the boiler itself, which reduces the availability of complicated 10 systems with intricate moving parts for interior boiler operations.

Accordingly, a continuing need exists for improved sootblowers and related automatic boiler cleaning systems for power plants. More specifically, a need exists for more effective cleaning systems for the platens in industrial boilers.

15 SUMMARY OF THE INVENTION

The present invention meets the needs described above in a multi-media rotating sootblower that includes multiple rotating and individually controlled cleaning fluid applicators, such a set of steam nozzles and two sets of water nozzles, and an automatic boiler cleaning system using these sootblowers. The boiler superheater 20 typically includes a system of these sootblowers to clean a number of large platens that are arranged in rows. The boiler may also include additional boiler cleaning equipment, including water cannons to clean the furnace, and conventional steam sootblowers to clean other heat exchangers of the boiler. A number of sensors, including heat transfer gauges that measure the heat transfer at the furnace wall, 25 strain gauges that measure the weight of slag deposits on platens, and boiler cameras are used to monitor slag accumulations within the boiler. A control system uses this sensor data to automatically operate the boiler cleaning system to implement an automatic boiler cleaning regimen, which maintains desired boiler thermal output and boiler life by cleaning the interior boiler components while avoiding 30 unnecessary thermal stress that can be caused by cleaning with water.

The multi-media rotating sootblower includes a lance that is linearly inserted into and retracted from the boiler interior while rotating, which deploys cleaning fluids in a corkscrew pattern. The lance typically includes a first set of water nozzles that point forward in the direction of lance insertion to clean one side of a platen as the 35 lances moves past the platen during the insertion pass, and a second set of water

nozzles that point rearward in the direction of lance retraction to clean the other side of the platen as the lances moves past the platen during the retraction pass. The forward pointing and rearward pointing nozzles are independently controlled so that each set can be independently turned off, while the other set remains in operation.

5 This allows the sootblower to clean with one set of nozzles while the other set is turned off to avoid damage as those nozzles pass close by other pendent structures, which permits the lance move through the superheater, effectively cleaning and passing close by platens without damaging them.

The control system closely controls the application of water as a cleaning fluid
10 to avoid imposing unnecessary thermal stress on the interior boiler structures. For example, the rotation speed of the lance may be controlled to produce a water stream with a constant progression rate on the boiler structure being cleaned, which varies in distance from the water nozzles as the lance travels through the superheater. This requires the lance to rotate more quickly when cleaning closer boiler structures, and
15 more slowly when cleaning structures that are further away. In addition, boiler cameras may be used to detect successful slag removal to ensure that water is applied to accumulated slag but not to bare platen tubes. Platen strain gauges and heat transfer gauges in the furnace section of the boiler also participate in the slag monitoring and automatic boiler cleaning regimen.

20 Using a single sootblower to apply different types of cleaning fluids minimizes the number of sootblowers required to implement a multi-media cleaning regimen. The multi-media capability of the lance also enables selective cleaning regimens designed to minimize the thermal shock to the boiler heat exchangers during the cleaning process. In particular, water can be used as a selective cleaning fluid for
25 slag encrusted areas, while steam can be use continuously in a cleaning operation. In addition, one fluid may be used to cool the lance during a dual-media cleaning operation. Specifically, steam application has the effect of cooling the lance while water is also applied by the lance. This prevents overheating of the lance, which allows a dual-media cleaning operation to be sustained longer than a water-only
30 cleaning operation could be sustained under similar boiler conditions. For similar reasons, and to keep the water nozzles from clogging with ash, the sootblower includes a pneumatic system for purging water from the lance and pumping air through the lance water system while steam is uses as a cleaning fluid. This prevents stagnant water in the lance from flashing to steam while the lance is in operation
35 inside the boiler, which cold rupture the water lines and destroy the lance.

Generally described, the invention may be implemented as a sootblower for cleaning internal components of a boiler while the boiler is in operation. The sootblower includes a lance tube having at least two separately controlled cleaning fluid applicators. The lance tube rotates as it delivers the separately controlled 5 cleaning fluids to clean the interior components of the boiler. The sootblower also includes a drive system for linearly inserting the lance tube into and retracting the lance tube from the boiler while rotating the lance tube, and a control system for controlling the delivery of the cleaning fluids.

More specifically, the sootblower typically applies steam as first cleaning fluid, 10 and includes a steam tube, on which the lance tube is telescopically received, that delivers steam into an interior cavity of the lance tube. The end of the lance tube typically includes one or more steam nozzles in fluid communication with the interior cavity of the lance tube for directing the steam out of the lance tube and into the boiler interior, and a steam valve controls the delivery of steam to the steam tube. The 15 sootblower also includes a carriage that is propelled by the drive system for telescopically inserting the lance tube into and retracting the lance tube from the boiler while the lance tube rotates and the steam tube remains stationary.

In addition, the sootblower typically applies water as the second cleaning fluid, either by itself or in combination with the first cleaning fluid, and includes a system of 20 water conduits located within the interior cavity of the lance tube for this purpose. A system of water nozzles in fluid communication with the water conduits directs water streams out of the lance tube and into the boiler interior. For example, the sootblower may include a first separately controlled water valve, water conduit and water nozzle system that is pointed toward the direction of lance insertion, and a second separately 25 controlled water valve, water conduit and water nozzle system that is pointed toward the direction of lance retraction. The sootblower also typically includes a water distributor carried by the carriage for delivering water from water supply devices, such as water hoses, to the water conduits while the water conduits rotate with respect to the water supply devices. The sootblower should also include a flexible link between 30 each water conduit and an associated water nozzle to adjust for different thermal expansion properties exhibited by the lance tube and the water conduits.

The sootblower may also include a rotation motor carried by the carriage for rotating the lance tube, and a linear travel motor carried by the carriage for inserting the lance into and retracting the lance from the boiler interior. The sootblower may 35 also include a frame supporting the steam tube and a toothed rack and a rail. The

sootblower also typically includes a roller coupled to the carriage and riding on the rail for supporting the linear travel of the carriage, and a pinion gear driven by the linear travel motor and engaged with the rack for driving the linear travel of the lance tube. The sootblower may also include a hose take-up tray supported by the frame and 5 providing a folding linkage that supports the water hoses, which feed the water distributor as the carriage moves along the steam tube.

The control system for the sootblower generally includes a system of strain 10 gauges measuring the accumulation of ash deposits on interior boiler components and automatically triggering operation of the sootblower to clean the components with steam, water or a combination of steam and water upon detection of predetermined 15 levels of accumulation. The control system may also be configured to control the rotation and linear motion of the lance tube to apply a substantially constant progression of the water and steam streams as they contact an internal boiler component. Further, the control system may include a system of boiler cameras viewing the interior boiler components and may automatically discontinue operation of 20 the sootblower to clean components, or portions of components, upon detection of successful cleaning. This avoids the application of water to bare heat exchangers, which could damage the tubes of the heat exchangers.

The invention may also be deployed as a power plant having a boiler with a 25 thermal output rating, and as an automatic cleaning system for the boiler configured to automatically clean the boiler to maintain the thermal output rating. The automatic cleaning system includes boiler monitoring equipment for detecting an ash accumulation condition of the interior of the boiler, and boiler cleaning equipment for cleaning the interior of the boiler while the boiler is in operation including at least one 30 multi-media rotating sootblower. The automatic cleaning system also includes a control system configured to receive sensor data from the boiler monitoring equipment, determine the ash accumulation condition of the interior of the boiler based on the sensor data, and to generate control signals to automatically activate and control the boiler cleaning equipment in response to the ash accumulation condition.

In view of the foregoing, it will be appreciated that the present invention avoids 35 the drawbacks of prior sootblowers for cleaning industrial boilers and provides an improved automatic boiler cleaning system. The specific techniques and structures for creating multi-media rotating sootblowers and associated automatic boiler cleaning systems, and thereby accomplishing the advantages described above, will become

apparent from the following detailed description of the embodiments and the appended drawings and claims.

BRIEF DESCRIPTION OF THE DRAWINGS

5 FIG. 1 is a conceptual illustration of a multi-media rotating sootblower.

FIG. 2A is a conceptual illustration of the multi-media rotating sootblower of FIG. 1 cleaning a first side of a superheater platen.

FIG. 2B is a conceptual illustration of the multi-media rotating sootblower of FIG. 2A cleaning an opposing side of the superheater platen.

10 FIG. 3A a rear side view of a multi-media rotating sootblower shown to scale and showing a pluming configuration of the sootblower.

FIG. 3B is a top view of the sootblower showing the pluming configuration.

FIG. 3C is an end view of the sootblower showing the pluming configuration.

FIG. 3D is an opposite end view of the sootblower.

15 FIG. 3E is a side view of the pluming configuration.

FIG. 3F is a top view of a portion of the pluming configuration.

FIG. 3G is an end view of the pluming configuration.

FIG. 4A is a Process Instrument Diagram for the sootblower of FIG. 3.

FIG. 4B is a legend for the Process Instrument Diagram of FIG. 4.

20 FIG. 5A is a block diagram of a power plant including an industrial boiler with an automatic cleaning system using multi-media rotating sootblowers.

FIG. 5B is a conceptual illustration of the boiler of FIG. 5.

FIG. 6 is a conceptual boiler side view showing a multi-media rotating sootblower illustrating the cleaning principle of constant water stream progression.

25 FIG. 7A is a conceptual boiler top view showing a multi-media rotating sootblower illustrating the cleaning principle of constant water stream progression to a first side of a platen.

FIG. 7B is a conceptual boiler top view showing a multi-media rotating sootblower illustrating the cleaning principle of constant water stream progression applied to the other side of the platen illustrated in FIG. 7A.

30 FIG. 8A is conceptual illustration of the use of water as a cleaning fluid in a slag removal process.

FIG. 8B is a continuation of the conceptual illustration of FIG. 8A.

FIG. 9 is block diagram illustrating a control system for an automatic boiler

35 cleaning system.

FIG. 10 is a side view of a multi-media rotating sootblower shown to scale.

FIG. 11 is a side view of the sootblower of FIG. 10 with the lance in a partially inserted position.

FIG. 12 is a side view of the sootblower of FIG. 10 with the lance in a fully 5 inserted position.

FIG. 13 is a perspective side view of the lance of the sootblower of FIG. 10.

FIG. 14 is a perspective side view of the lance of FIG. 13 with the outer housing removed.

FIG. 15 is a perspective side view of the flexible connectors and nozzles 10 located at the end of the lance of FIG. 13.

FIG. 16 is a side view of the flexible connectors and nozzles of FIG. 15.

FIG. 17 is a perspective, exploded side view of the water distributor of the sootblower of FIG. 10.

FIG. 18 is a perspective, exploded side view of the water distributor of FIG. 17 15 shown from a different perspective.

FIG. 19 is a perspective, exploded side view of the water distributor of FIG. 17 with the outer housing of the water distributor removed.

FIG. 20 is an exploded side view of the water distributor of FIG. 17 with the outer housing of the water distributor removed.

20 FIG. 21 is side crosssection view of the water distributor of FIG. 17 showing a first water channel in fluid communication with a first set of water conduits.

FIG. 22 is a side crosssection view of the water distributor of FIG. 21 showing a second water channel in fluid communication with a second set of water conduits.

FIG. 23 is perspective view of the carriage of the sootblower of FIG. 10.

25 FIG. 24 is perspective view of the other side of the carriage of FIG. 23.

FIG. 25 is bottom view of the carriage of FIG. 23.

FIG. 26 is top view of the carriage of FIG. 23.

FIG. 27 is side view of the drive system of the sootblower of FIG. 10.

FIG. 28 is perspective rear view of the drive system of FIG. 27.

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DETAILED DESCRIPTION OF EXEMPLARY EMBODIMENTS

The present invention relates to a multi-media rotating sootblower and associated automatic boiler cleaning systems. In general, the sootblower selectively applies two cleaning fluids, typically water and steam, which may be applied 35 individually or in combination during a cleaning operation. However, the principles

realized by the exemplary embodiments of the invention as described in this specification may be directly modified and extrapolated to develop sootblowers capable of applying more than two independently controlled cleaning fluids, having more than two independently controlled systems for applying any particular cleaning 5 fluid, and for applying different types of cleaning fluids, such as air, solvents, sand blast streams, bead blast streams, liquid nitrogen or other very cold fluids, superheated plasma or other very hot fluids, or any other cleaning fluid that may be appropriate for a particular application. It should also be appreciated that the sootblower may be used for purposes other than cleaning, such as applying paint, 10 sealant, or other desired coatings to interior boiler components.

The exemplary sootblower described below also includes two independently controlled water application systems, which each include two nozzles. Of course, the number of independently controlled water systems, and the number of nozzles included in each water application system, are design choices that may be altered to 15 meet the objectives of a particular application. Similarly, the exemplary sootblower includes a single steam application system with two nozzles, but additional steam systems and different numbers of steam nozzles may be included, as desired, for particular applications.

The particular multi-media rotating sootblower and associated automatic boiler 20 cleaning system described below are well adapted for use in large-scale coal-fired, oil-fired and trash-fired boilers that are typically used to generate electric power and heat or process steam for industrial enterprises, such as electricity generation, paper manufacturing and municipal incineration. Nevertheless, it should be understood that these or modified sootblowers may also be used in other types of industrial boilers, 25 such as wood, straw, peat and manure-fired boilers, as well as heat recovery boilers commonly used in steel and aluminum smelters, chemical manufacturing, oil refineries, and other industrial processes. Basically, all industrial boilers can benefit from effective cleaning, and a variation of the multi-media rotating sootblower described below may be readily adapted to any particular industrial boiler 30 configuration and cleaning requirement.

It should also be understood that many design modifications and additions may be readily deployed with the particular commercial embodiment described below, such as independently articulating and controlled nozzles, articulating lances (which are described below as rotating and linearly traveling, but not otherwise articulating), 35 pulsating cleaning fluid streams, varying pressure cleaning fluid streams, alternating

cleaning media fluid streams, and so forth. However, each of these modifications would add cost and complexity to the system. Therefore, it should also be appreciated that the preferred sootblower described below is presently considered by the inventors to embody the most technically and economically feasible sootblowers for today's industrial boilers, and in particular the boilers found in oil-fired, coal-fired and trash-fired boilers in power plants used for electricity generation and waste incineration, as well as boilers used in paper manufacturing, oil refining, steel and aluminum smelting.

Turning now to the figures, in which similar reference numerals indicate similar elements in the several figures, FIG. 1 is a conceptual illustration of a multi-media rotating sootblower 10, which shows the major components of an illustrative embodiment of the present invention. This particular embodiment of the invention includes a single rotating and linearly traveling lance tube 12 that carries a separately controlled steam application system along with two separately controlled water application systems. More specifically, the lance tube 12 is telescopically mounted on a steam tube 14, which is mounted to a fixed frame 16. The frame may also include a two or three-sided hood positioned above the lance and steam tube assembly, in which case it may be referred to as a "canopy." The frame, in turn, is ordinarily welded or bolted in place adjacent to the outer wall 18 of an industrial boiler, with the nozzle end of the lance tube 12 positioned for insertion into the boiler at a desired cleaning location. The lance tube 12 is typically inserted through an opening 19 in the boiler wall 18 that is regulated by a wall box 20, which maintains a seal between the boiler wall and the lance tube while the lance rotates and moves into and out of the boiler. In some boiler configurations, particularly those operating with positive boiler pressure (i.e., internal boiler pressure above one atmosphere) the lance may be configured to extend into the wall box in the fully retracted position to plug the opening in the boiler wall, which may also include a auxiliary cover. In other configurations, particularly those operating with negative boiler pressure, the lance may be removed from the wall box as shown in FIG. 1 when the lance is in the fully retracted position.

The rear end of the lance tube 12 is mounted to a carriage 22, which is supported by a pair of rollers (only one roller 24 is shown in FIG. 1) that each ride along the top side of a support rail (only one support rail 26 is shown in FIG. 1) mounted to the frame 16. The carriage also supports a linear travel motor 28, which is also called an insertion motor, that drives a pair of pinion gears (only one pinion

gears **30** is shown in FIG. 1). The pinion gears **30**, in turn, each engage a toothed rack (only one toothed rack **32** is shown in FIG. 1), which are also supported by the frame **16**. The carriage also supports a rotation motor **34** that rotates the lance tube **12** about the steam tube **14** as the linear travel motor **28** drives the pinion gears **30** to 5 telescopically move the lance tube **12** along the steam tube **14**. That is, the lance tube **12** rotates about and travels telescopically along the steam tube **14**, which is supported by the frame **16** and remains stationary. It should be appreciated that the 10 rotation and linear travel motors, as well as the rollers, rails, rack and pinion gear assembly may be located in positions other than as shown in FIG. 1. In particular, the carriage **22** may be configured to hang from an overhead canopy-style frame **16**, in which case the rollers, rails, rack and pinion gear assembly may be located to the side or above the carriage. See in particular the commercial embodiment illustrated 15 with reference to FIGS. 10-28.

The independently controlled steam application system includes a steam supply **36** provided to a steam valve **38** that controls the introduction of steam into the 20 end of the steam tube **14** located near the carriage **22**. The steam valve **38** is typically operated manually, although the computer controller **40** could alternatively be configured to control the operation of the steam valve for automatic and remotely-controlled operation. A linkage **42** connected to the carriage **22** engages a lever located on the steam valve **38** to manually lock the steam valve in a closed position 25 when the carriage **22** is in the fully retracted position. The opposing end of the steam tube **14** is open, which allows steam to fill and pressurize the interior cavity of the lance tube **12** with steam whenever the steam valve **38** is open. The interior cavity of the lance tube **12**, in turn, is in fluid communication with a pair of nozzles, which are 30 also called steam jets (only one steam jet **44** is shown in FIG. 1). In this particular embodiment, the steam jets have a fixed pointing angle, typically pointing slightly forward in the direction of lance insertion. This pointing angle is a design choice that may be altered by adjusting or changing the steam jets. This arrangement allows the steam tube **14** to inject steam into the lance tube **12** while the lance tube rotates about and telescopes along the steam tube.

The first independently controlled water application system includes a water valve **45** regulating water delivery from a water supply **46** to a water-1 hose **48**, which is connected to a first water inlet (element **150** shown on FIG. 10) on a water distributor **50**. The water distributor **50** travels linearly with the carriage **22** and 35 includes an outer housing that remains rotationally stationary while an inner sleeve

rotates with the lance 12. The water distributor 50 also defines a first pressurized water channel (including elements 160 and 180 shown on FIG. 21) that directs water from the rotationally fixed first water inlet 150 in the outer casing of the water distributor into a pair of water-1 conduits 52 (only one water-1 conduit is shown in FIG. 1). This allows the water distributor 50 to supply water from the water-1 hose 48 to the water-1 conduits 52 while the conduits rotate with respect to the water-1 hose, which remains connected to the non-rotating outer casing of the water distributor. The water-1 conduits 52 connect the water supply 46 to a pair of nozzles or water-1 jets 54 (only one water-1 jet is shown in FIG. 1) located at the opposite end of the lance tube 12. That is, a second water-1 conduit 52 (not shown) also connects the water supply 46 to a second water-1 jet 54 (not shown), which is typically positioned in the same linear position on the opposite side of the lance tube 12. Both of the water-1 jets 54 are typically pointed forward in the direction of lance insertion. A water-1 valve 45, which is typically located on the back side of the frame 16 but may be located in any suitable location in the pluming system, controls the flow of the first water supply 46 into the water-1 conduits 52 under the control of the controller 40.

The second independently controlled water application system is similar to the first, and includes a second water valve 55 regulating the supply of water from the water supply 46 to a water-2 hose 58, which is connected to a second water inlet (element 152 shown on FIG. 10) on the water distributor 50. The water distributor 50 defines a second pressurized water channel (including elements 170 and 182 shown on FIG. 22) that directs water from the rotationally fixed second water inlet 152 in the outer casing of the water distributor into a pair of water-2 conduits 62 (only one water-2 conduit is shown in FIG. 1). This allows the water distributor 50 to supply water from the water-2 hose 58 to the water-2 conduits 62 while the conduits rotate with respect to the water-2 hose, which remains connected to the non-rotating outer casing of the water distributor. The water-2 conduits 62 connect the water supply 46 to a pair of nozzles or water-2 jets 64 (only one water-2 jet is shown in FIG. 1) located at the opposite end of the lance tube 12. That is, a second water-2 conduit 62 (not shown) also connects the water supply 46 to a second water-2 jet 64 (not shown), which is typically positioned in the same linear position on the opposite side of the lance tube 12. Both of the water-2 jets 64 are typically pointed rearward in the direction of lance retraction. A water-2 valve 55 typically located on back side of the frame 16 controls the flow of the second water supply 46 into the water-2 conduits 62 under the control of the controller 40. A pluming system feeding the water valves and

a pneumatic system 72 are also typically located on the back side of the frame 16 (see FIGS. 3A-G and 4A-B) but may be located in any other suitable location.

The water and steam jets are mounted in a multi-media nozzle 66, which typically has the same diameter as the lance tube 12 to facilitate entering the lance tube into the boiler through the opening 19 through the boiler wall 18. The water-1 and water-2 conduits are preferably connected to the multi-media nozzle 66 with flexible connectors 68, such as corrugated steel tubes, to allow for different thermal expansion rates between the lance tube 12 and the water conduits. The sootblower 10 also includes a hose take-up tray 70 that includes a number of box links that form a chain that supports the water hoses 48, 58. The hose take-up tray 70 also carries electric cables for powering and controlling the electric components carried by the carriage 22, including the rotation motor 34 and the linear travel motor 28. The take-up tray 70 is configured to fold back in an adjustable-length loop while remaining sufficiently rigid to support the water hoses 48, 58 and the electric cables while the carriage 22 moves back and forth along the steam tube 14.

FIG. 2A is a conceptual illustration of the multi-media rotating sootblower 10 cleaning a first side 80 of a superheater platen 82. The configuration of the platens with respect to the lance during a typical cleaning operation is also shown in FIGS. 6 and 7A-B. The lance sprays a water-1 stream 84 from the water-1 jet 54, which is pointed forward in the direction of lance insertion. As noted previously, the lance 12 rotates as it travels linearly, which causes the water-1 stream 84 to advance in a corkscrew pattern. Therefore, the portion of the platen side 80 cleaned by the water-1 stream 84 gets closer to the lance 12 as the lance approaches the platen 82. The water-1 stream 84 typically cleans a pair of rows of parallel platens during an insertion pass, with one row of platens located on opposing sides of the lance insertion path (see FIGS. 7A-B). The water-2 stream 86 subsequently cleans the back sides of the same platens during a retraction pass. This is illustrated in FIG. 2B, in which the water-2 stream 86 is shown cleaning the back side 88 of the platen 82. Of course, a steam spray 90 may alternatively or additionally be used to clean either or both sides of the platen 82. For example, the steam spray 90 may be used to clean the platen 82 several times a day or hourly, whereas water cleaning may be applied selectively to slag-encrusted areas platen on an as-needed basis or according to a less frequent regularly-scheduled cleaning regimen.

FIGS. 3A-G and 10-28 include three-dimensional computer-assisted design (CAD) illustrations of a specific commercial embodiment of the multi-media rotating

sootblower 10 shown to scale (excluding the fan 302, which is shown conceptually). This commercial embodiment represents the best mode currently known by the inventors for practicing this aspect of the invention, and the dimensions shown are typical for an industrial sootblower. However, the particular dimensions are design 5 choices that will change based on the particular portion of the particular boiler that the sootblower is designed to clean.

FIG. 3A a side view of the sootblower 10 showing a pluming configuration 300, which feeds the water hoses 48, 58 described with reference to FIG. 1. The sootblower 10 also includes a pneumatic fan 302 that provides low pressure air for 10 sealing the wall box 20 and forcing a constant flow of air through the sootblower water system to prevent boiler gasses from enter the water nozzles during steam blowing. It is desirable to run air through the water system of the sootblower whenever the lance is in operation without applying water. The constant flow of low pressure air from the fan 302 cools the lance and prevents the water nozzles from clogging with 15 ash. Therefore, air from the fan 302 is normally run through the lance when steam, but not water, is being used as a cleaning fluid. In addition, high pressure air, typically from an on-site plant pneumatic system or air compressor, is used to flush the water form the water system. It is important to flush the water from the lance after 20 water is used as a cleaning fluid to prevent the water from dripping out of the lance when parked. It is also desirable to flush the water system to prevent stagnant water in the lance tube from overheating while the lance is inside the boiler, which could cause the water to flash to steam and rupture the conduits inside the lance tube.

In figures 3A-E, the tubes of the pneumatic system are not shown to reduce clutter. However, the pneumatic pluming itself is conventional and represented on the 25 Process Instrumentation Drawing of FIGS. 4A-B. FIG. 3B is a top view of the sootblower 10 showing the pluming configuration 300, and FIGS. 3C and 3D are end views of the sootblower showing the pluming configuration. FIG. 3E is a closer side view of the pluming configuration 300. The water supply 46 is connected to a main manual water shut-off valve 304. The pluming then proceeds through a strainer 306 30 to a "T" splitter 308, which is fitted with a water pressure gauge 310. From the splitter, one pipe goes to the water-1 valve 45 and another pipe goes to the water-2 valve 55. The water-1 valve 45 includes a locally-controlled pneumatic valve 310 and a remotely-controlled pneumatic valve 312 equipped with a computer-controlled actuator operated by the control system 40 (shown on FIGS. 1 and 9). From the 35 water-1 valve 45, the pluming continues through a pneumatic inlet 318, which is

connected to the pneumatic system **72** for purging the water from and running air through the sootblower water system, to a 90 degree turn **322**, which passes through the frame **16** to a connection for the water-1 hose **48**.

The second pluming line is similar, and includes a locally-controlled pneumatic valve **314** and a remotely-controlled pneumatic valve **316** for the water-2 valve **55** equipped with a computer-controlled actuator operated by the control system **40**. From the water-2 valve **55**, the pluming continues through a pneumatic inlet **320** connected to the pneumatic system **72** to a 90 degree turn **324**, which passes through the frame **16** to a connection for the water-2 hose **58**. The pluming system **300** is mounted to the frame **16** by four channel brackets **340**. FIG. 3F is a top view of the 90 degree turns **322**, **324** passing through the frame **16**, and FIG. 3G is an end view of the pluming configuration **300**.

FIG. 4A is a Process Instrument Diagram (PID) for the sootblower **10**, which illustrates the pluming system **300** and the associated pneumatic system **350** along with electrical connections to the controller **40** (labeled PLC in FIG. 4A). The fan **302** provides low pressure air to seal the wall box **20** and feed air through the water system of the sootblower **10**. As noted previously, this air is used to prevent boiler gasses from entering the water nozzles and to prevent the water nozzles from clogging with ash. The pneumatic system **350** also includes a plant air source **342**, which provides high-pressure air for purging the water from the lance after a water blowing cycle. The plant air source **342** also provides instrument air **352** for operating the pneumatically-controlled water valves **45**, **55**. The remaining elements of the pluming system **300** and the associated pneumatic system **350** are conventional and denoted by their usual symbols in FIG. 4A. FIG. 4B is a legend for the PID of FIG. 4.

FIG. 5A is a block diagram of a power plant **91** including an industrial boiler **102** with an automatic cleaning system **100** that includes a system of strategically placed multi-media rotating sootblowers **10**. The power plant **91**, which is intended to represent any of a wide range of industrial power plants, generally includes steam-driven equipment **93**, such as a steam turbine and electric generator in the case of an electricity plant, a pulp cooker in the case of a paper manufacturing plant, or other equipment driven by steam created by the boiler **102**. The power plant also generally includes water cooling and recirculation equipment **94**, ash collection and disposal equipment **97**, and fuel handling equipment **98**. Except for the automatic boiler cleaning system **100**, the industrial boiler **102** is conventional and, therefore, will not be described in detail.

It should be appreciated that the output rating of the power plant 91, such as its MW-electric rating in the case of an electricity plant, relies on the thermal output of the boiler 102, which is typically expressed as a MW-thermal rating. Further, accumulated ash and slag in the boiler 102 reduces the heat transfer capability of the 5 heat exchangers within the boiler, which reduces the thermal output of the boiler, which reduces the efficiency of the power plant 91. If the heat transfer capability is not regularly restored through an effective cleaning regimen, the output rating of the power plant 91 may be reduced, which would be a very expensive consequence for the owner of the plant. For this reason, the output ratings of the boiler and power 10 plant both depend on an effective cleaning regimen for the boiler 102. The boiler life also depends on a cleaning regimen that minimizes the thermal shock imposed on the heat exchanger tubes during the cleaning process. The automatic boiler cleaning system 100, which includes a system of strategically placed multi-media rotating sootblowers 10 along with boiler monitoring equipment and a control system, 15 implements such a cleaning regimen to maintain the thermal output rating of the boiler and the electric output rating of the power plant 91 at the desired levels while minimizing the thermal shock imposed on the heat exchanger tubes within the boiler during the cleaning process. .

FIG. 5B is a conceptual illustration of the industrial boiler 102, which includes 20 the automatic boiler cleaning system 100. FIG. 9 also shows a block diagram illustrating a control system 40 for the automatic boiler cleaning system 100. The boiler 102 structure is typically in the range of about 150 to 250 feet [about 45 to 75 meters] tall. Generally described, the boiler includes an open furnace section 104 housed within walls constructed from heat exchanger tubes, represented by the heat 25 exchanger tube 106, which carry pressurized water heated by the furnace. An ash collection and disposal section 108 is located below the furnace, which collects ash as it is created in the furnace section 104 during the combustion process in a hopper and transports it away from the boiler for disposal, typically using a conveyor or rail car. A platen superheater section 110 is located directly above the furnace, which 30 includes a number of platens constructed from heat exchanger tubes that hang from the boiler roof section 112, suspended above the combustion zone within the furnace 104. The boiler 102 also includes a number of lower-temperature heat exchangers identified as the convection zone 111, which in this example includes a pre-heater 113, a primary superheater 115 and an economizer 117.

The boiler monitoring equipment includes a number of strain gauges, as represented by the strain gauge **114**, that measure the weight of the platens, which increases as slag accumulates on the platens. Typical strain gauges of this type are described in Jones, U.S. Patent No. 6,323,442, which is incorporated herein by reference. A number of boiler cameras, as represented by the boiler camera **116** (boiler cameras are denoted by squares) are strategically located with the boiler to view to the platens and other heat exchangers. In addition, the boiler tubes in the furnace section **104** typically include a number of in-line heat transfer gauges, as represented by the illustrative heat transfer gauge **118** shown in-line with the heat exchanger tube **106**, which measure the heat transferred from the furnace to the heat exchanger tubes in the furnace wall. The boiler camera **116** and heat transfer gauge **118** are conventional, and will not be described further. It should also be understood that the particular number and locations of boiler cameras and transfer gauges shown in FIG. 5 are merely illustrative, and will vary from application to application.

The boiler cleaning equipment typically includes a number of multi-media rotating sootblowers **10** (multi-media rotating sootblowers are denoted by circles) positioned to clean the platen section **110**. The number of multi-media rotating sootblowers **10** deployed in any particular plant will vary from plant to plant, and will be based on cost and other considerations. In addition, typically about 4 to 8 water cannons, as represented by the water cannon **120**, are typically positioned to clean the furnace section **104**. Further, typically about 10 to 20 single-media sootblowers **122** (e.g., water or steam sootblowers, which are denoted by triangles) are also positioned to clean the lower-temperature heat exchangers **113**, **115** and **117**. Again, it should be understood that the number and locations of sootblowers and water cannons shown in FIG. 5 are merely illustrative, and will vary for each application.

The control system **40** shown on FIGS. 1 and 9 controls the boiler cleaning equipment **10**, **120**, **122** in response to sensor data received from the boiler monitoring equipment **114**, **116**, **118** to attain control objectives designed to implement selective cleaning while minimizing thermal shock to the heat exchangers. In particular, the control system **40** operates the multi-media rotating sootblowers **10** to maintain constant water and stream progression velocity, as described with reference to FIGS. 6 and 7A-B. The control system **40** also uses sensor data from the boiler cameras **116** to implement selective cleaning to minimize water shock, as described with reference to FIG. 8.

FIG. 6 is a conceptual boiler side view showing a multi-media rotating sootblower 10 illustrating the cleaning principle of constant water stream progression. During the cleaning process, the lance tube 12 approaches the platen 82, which typically includes a face 80 to be cleaned positioned perpendicular to and adjacent to the lance tube insertion path. This arrangement is also shown in a boiler top view (plan view) in FIGS. 7A and 7B. Because the angle of the water-1 stream 84 is fixed with respect to the lance 12, the portion of the platen face 80 contacted by the water-1 stream moves closer to the lance as the lance approaches the platen. Therefore, to keep the progression rate of the water-1 stream 84 constant on the platen face 80, the rotational speed of the lance 12 increases as the lance approaches the platen face. The linear insertion rate of the lance 12 may also be varied in this process. Furthermore, the water-1 stream 84 is typically turned off as the water-1 jet 54 passes close by the edge of the platen 80 to avoid damaging the platen. As shown in FIG. 7B, a similar cleaning operation is applied to the rear side 88 of the platen 82 during the return pass. Moreover, two rows of parallel platen panels are typically cleaned by a single sootblower, as shown conceptually in FIGS. 5 and 7A-B. This cleaning operation of the lance 12 may be governed automatically by the controller 40, or it may be controlled in real time by an operator monitoring the cleaning process with the system of boiler cameras 116.

FIGS. 8A-B are conceptual illustrations of the use of water as a cleaning fluid in a slag removal process. As shown in FIG. 8A, the lance 12 sprays a water stream on a slag accumulation 90. The water then soaks into the slag 90, which increases in temperature as it penetrates closer to the platen surface 80. Eventually, as shown in FIG. 8B, the water penetrates the slag 90 to a point at which it flashes to steam, which typically causes the slag to break away in fairly large chunks, as represented by the slag chunk 92. Once the chunk has been removed, the bare platen surface 80 is exposed. At this point, spraying the bare platen surface 80 with water would subject the platen to extreme and unnecessary water shock because the surface has already been successfully cleaned. To prevent such unnecessary water application, which could shorten the life of the boiler, the boiler camera 116, which may include an infrared or other sensor to detect slag removal, monitors the cleaning process, and the controller 40 uses sensor data from the boiler camera 116 to automatically discontinue cleaning of the portion of the platen surface 80 that has been successfully cleaned. This is quite important as a mechanism for avoiding unnecessary shock during the cleaning process. It should be understood that sensor data, as that term is

used in this specification, may include image data from the boiler cameras as well as infrared sensor data from the boiler cameras, heat transfer data, strain gauge data, and any other sensor data that may be available from any other instruments located in or monitoring the function of the boiler.

5 FIG. 10 shows a side view of the multi-media rotating sootblower 10 with the lance 12 carrying the multi-media nozzle 66 in a fully retracted position. This view also shows the frame 16 (also called a canopy), support rail 26 and the toothed rack 32. The water distributor 50 is also shown, with water inlets 150, 152 for the water hoses 48, 58 (see FIG. 1 -- the hoses themselves are not shown in FIGS. 10-28 for 10 clarity). The hose take-up tray 70 is also shown in this view, as is the steam valve 38, the linear travel motor 28, the rotation 34, and the extreme rear portion of the steam tube 14. This view also shows a packing assembly 35 that maintains a seal between the carriage 22 and the steam tube 14 to prevent steam from leaking during the cleaning operation. An exemplary packing assembly 35 is described in commonly-owned U.S. Patent Application Serial No. _____, entitled "Integral 15 Packing Housing and Packing Material Unit," filed contemporaneously with the present application, which is incorporated herein by reference. The sootblower 10 also includes an appropriate gasket between the packing assembly 35 and the spindle 190. For example, a copper gasket performs well in this application.

20 FIG. 11 is a side view of the sootblower 10 with the lance 12 in a partially inserted position. This view shows the components of the carriage 22, which travels linearly along with the rear of the lance 12 as the lance telescopes along the steam tube 14. In this view, the water hoses 48, 58 and the hose take-up tray 70 have been removed to lessen the clutter of the illustration. FIG. 12 shows the sootblower 10 with 25 the lance 12 in the fully inserted position.

FIG. 13 is a perspective side view of the lance 12, and FIG. 14 shows the lance with the outer housing removed to reveal one of the water-1 conduits 52 and one of the water-2 conduits 62. This view also shows the flexible connectors 68, which provide the water conduits 52, 62 with length adjustment to compensate for 30 different thermal expansion properties of the lance 12 and the water conduits. It should be appreciated that the water conduits are exposed to the temperature of steam within the lance, whereas the lance is exposed to the inter boiler temperature, which is much higher than the steam temperature. This sets up a rather severe thermal differential while the lance is operation inside the boiler. In addition, it is 35 desirable to run steam through the lance continuously during the cleaning operation,

even when water is the primary cleaning fluid being applied, because the constant steam flow cools the lance. For the same cooling purpose, and to keep ash from clogging the water nozzles, it is desirable to run air through the lance water system when steam is applied as the cleaning fluid.

5 FIG. 15 is a perspective side view of the flexible connectors 68 and multi-media nozzle 66 located at the end of the lance 12. The steam jet 44, the water-1 jet 54 and the water-2 jet 64 are shown in this view. FIG. 16 is a side view of this same portion of the sootblower 10. FIG. 17 is a perspective, exploded side view of the water distributor 50, which delivers water received at the water-1 inlet 150 from the water-1 10 hose 48 to the water-1 conduits 52 while the water-1 conduits rotate with the lance 12 and the water-1 inlet remains rotationally stationary. Similarly, the water distributor 50 delivers water received at the water-2 inlet 152 from the water-2 hose 58 to the water-2 conduits 62 while the water-2 conduits rotate with the lance 12 and the water-2 inlet remains rotationally stationary. FIG. 18 shows the water distributor 50 from a 15 different perspective.

FIG. 19 shows the water distributor 50 with the outer housing removed, which reveals a first water supply channel 160 that becomes pressurized with water supplied by the water-1 hose 48 through the water-1 inlet 150. Water within the first water supply channel 160 is forced through an opening 162 into a first pair of internal 20 conduits 180 (shown in FIG. 21) that are fluidly connected to the flange 166, which includes openings 168 that are fluidly connected to the water-1 conduits 52. This allows the water-1 conduits 52 to be pressurized with water received at the water-1 inlet 150 while the water-1 conduits rotate with the lance 12 and the water-1 inlet remains rotationally stationary. Similarly, a second water supply channel 170 25 becomes pressurized with water supplied by the water-2 hose 58 through the water-2 inlet 152. Water within the second water supply channel 170 is forced through an opening 172 into a second pair of internal conduits 182 (shown in FIG. 22) that are fluidly connected to the flange 176, which includes openings 178 that are fluidly connected to the water-2 conduits 62. This allows the water-2 conduits 62 to be 30 pressurized with water received at the water-2 inlet 152 while the water-2 conduits rotate with the lance 12 and the water-1 inlet remains rotationally stationary. FIG. 20 is a side view of this same structure.

FIG. 21 is side crosssection view of the water distributor 50, which illustrates the water-1 inlet 150 in fluid communication with the first water supply channel 160, 35 which is fluidly connected with the first pair of internal conduits 180, which supply

water to the water-1 conduits 54. Similarly, FIG. 22 is side crosssection view of the water distributor 50 showing the water-2 inlet 152 in fluid communication with the second water channel 170, which is fluidly connected with the second pair of internal conduits 182, which supply water to the water-2 conduits 64. FIG. 23 is perspective 5 view of the carriage 22 of the sootblower 10. This view shows a more detailed view of the water distributor 50, the packing assembly 35, the steam valve 38, the linkage 42, the linear travel motor 28, the rotation motor 34, the roller 24 and the pinion gear 30. This view also shows a chain linkage assembly 191 that translates rotation of the 10 rotation motor 34 to a spindle 190 (shown better in FIG. 25) located within a spindle housing 192 at the end of the lance 12, which rotationally drives the lance. FIG. 24 is perspective view of the other side of the carriage 22, which shows the same components from the other side. This view also shows spindle flange 193 that connects the spindle 190 to the rotating inner sleeve of the water distributor 50. This view also shows an angle bar 194 that mounts the rack 24 to the frame 16 (not shown 15 in this view).

FIG. 25 is bottom view of the carriage 22, which shows that there are two rails 26 and two racks 32 guiding the linear travel of the carriage. This view also shows the spindle 190 and the spindle housing 192 as well as two side roller supports 195 that support two side rollers 196 that ride against the inner sides of the guide rails 26 20 to limit lateral movement of the carriage 22. FIG. 26 is top view of the carriage 22, which provides a view of a portion of the hose take-up tray 70 and the frame 16. FIG. 27 is side view of the drive system of the sootblower 10, which provides a more detailed view of the rail 26, the roller 24 and the side roller 196 as they interact in the 25 drive system. FIG. 28 is perspective rear view of the drive system of the sootblower 10, which shows the support rail 26, roller 24 and side roller 196, as well as the rack 32 and pinion gear 30.

All of the following parameters are for a typical commercial sootblower 10 as shown and described with reference to FIGS. 10-28. These particular parameters may be varied for particular applications. The length of the lance tube 12 is about the 30 same as the frame 16, the steam tube 14, the support rail 26 and the toothed rack 32, which all correspond to the desired insertion length of the lance tube into the boiler. This length may vary from boiler to boiler, and may also vary from location to location 35 within a particular boiler. Lance lengths of 10 feet [3 m] to over 50 feet [15 m] are not uncommon. The steam supply 36, which has been used in sootblowers for years, may be any conventional industrial process steam, which is typically applied with a

nozzle velocity above the speed of sound. The water-supply **46** is typically in the area of 20 to 100 GPM [750 to 3,750 cm³/min] at pressures around 100 to 500 PSI [7 to 35 kg/cm²].

The frame **16** is typically constructed from formed carbon steel plates. The lance tube **12** is typically constructed from 1/8 to 1/2 inches [3.2 to 12.7 mm] thick steel tubing 5 to 6 inches [125 to 150 mm] in diameter. The steam tube **14** is typically constructed from 0.188 inches [4.8 mm] side-wall steel tubing 2 3/8 to 2 3/4 inches [60 to 70 mm] in diameter. The water hoses **46**, **56** are standard 3/4 inches [19 mm] diameter high-pressure hose, such as model number 100R12 manufactured by Ryco.

The water conduits **52**, **62** are typically constructed from 0.035 inches [0.89 mm] side-wall steel tubing 3/4 inches [19 mm] inches in diameter, and the flexible links **68** are typically 3/4 inches [19 mm] corrugated steel tube wrapped by steel mesh, such as model number UFBX1 manufactured by Senior Flexonics.

The rotation motor **34** and the linear travel motor **28** may be a brushless DC servo motor, such as the PMA57R model manufactured by Pacific Scientific providing a 195 lb-in (22.0 Nm) continuous torque. The hose take-up tray **70** may be a model number 340-100-150 manufactured by Igus. The roller **24**, the pinion gear **30**, and the rack are a custom manufactured items milled from steel. The controller **40** may be any suitable type of industrial programmable logic type controller, such as a the ControlLogix models manufactured by Allen Bradley. For boilers operating with positive pressure, the pneumatic fan **302** may be a Becker type SV 7.330 rated for 60 Hz, 230/400 V, 4.8 KW. This fan will be suitable, but a somewhat smaller fan may be specified for boilers operating with negative pressure.

The steam valve **38** may be a typical, mechanically or pneumatically operated shut off valve as commonly used on sootblowers and manufactured from cast steel, and the water valves **55**, **65** may be model number VSV-F 50 NC manufactured by COAX. The multi-media nozzle is a custom manufactured item, which is typically manufactured from heat resistant stainless steel milled to the desired specifications and welded or threaded into to the end of the lance tube **12**. The carriage **22** is a also custom manufactured item, which is typically manufactured form cast iron milled to the desired specifications. The wall box **20** is another custom manufactured item, and consist of an outer tube and a sealing device, such as a conventional pressure-loaded packing. The linkage **42** is a standard item that has been included on conventional steam sootblowers for may years.

In view of the foregoing, it will be appreciated that present invention provides significant improvements in sootblowers and automatic boiler cleaning systems and that numerous changes may be made therein without departing from the spirit and scope of the invention as defined by the following claims.